

# **Free Study Material from All Lab Experiments**



**Thermodynamics Notes  
for NET/GATE Physical Sciences  
# Thermodynamic Potentials #**

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## GIBB'S FREE ENERGY

COMPT<sup>II</sup>(T, P)

- It is a Extensive property.
- It is a State function.
- It is a form of Energy which can be used in any useful work
- ↓ in free Energy is use as a non-mechanical work
- Its unit is Joule
- mathematical it can be written as

$$G = H - TS$$

where  $H$  is a total Energy of a System  
where  $TS$  is Unavailable Energy.

[Or U can say that disorder can't ever be use as a work, bcoz u need this energy the substance change their phase]

- Derivation of Maxwell Equation in term of  $G$ .

$$G = H - TS$$

$$G = U + PV - TS \quad [H = E + PV]$$

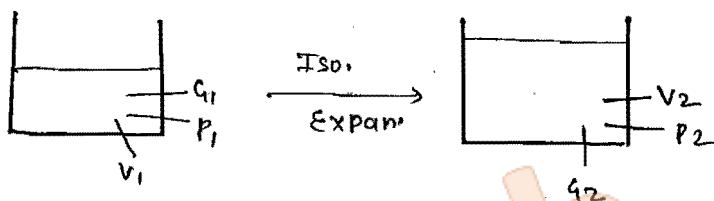
Diffr. both side

$$dG = dE + PDV - TdS - SdT + VdP$$

$$\therefore dE = dq - PDV$$

$$dE = TdS - PDV$$

→ Calculation of change in free energy for an isothermal process in the case of ideal gas →



we know that -  
from maxwell Equ"

$$\left(\frac{\partial q}{\partial p}\right)_T = v$$

$$dq = v dp \quad [ \because PV = RT ]$$

$$v = \frac{RT}{P}$$

$$\Delta G = RT \int_{P_1}^{P_2} \frac{dp}{d}$$

$$\Delta G = RT \ln \frac{P_2}{P_1}$$

(Gout-2009)

Ass. ⑪

Q4.32

$$\Delta G$$

$$n = 1$$

$$P_1 = 1 \text{ atm}$$

$$P_2 = 2 \text{ atm}$$

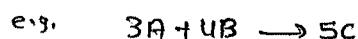
$$\Delta G = RT \ln \frac{2}{1}$$

$$\Delta G = RT \ln 2$$

⇒ Calculation of  $\Delta G$  for a reaction.

Imp

$$\Delta G = \sum G_{\text{PRODUCT}} - \sum G_{\text{REACTANT}}$$



A  $G_1 \Rightarrow J/\text{mole}$

B  $G_2 \Rightarrow J/\text{mole}$

C  $G_3 \Rightarrow J/\text{mole}$

$$\Delta G = 5G_3 - 4G_2 - 3G_1$$

For Spontaneous process  $\Delta G$  always be -ive -

$$\Delta G = \Delta H - T\Delta S$$

∴  $\Delta S$  always be positive

∴  $\Delta H$  ~~also~~ may be positive or negative

∴  $\Delta G \rightarrow$  {always Negative}

[ $\Delta G$  को -iv लेने के लिये

$\Delta H$  की value ~~T~~ S से

छोटी होनी चाहिए

H

\* Prove that for Spontaneous process  $\Delta G$  is less than zero  
(Isochoric proc.)

We know that the heat change in a reversible process is more than the heat change in a irreversible process.

$$dq_{\text{rev.}} > dq_{\text{irrev.}}$$

$$T ds > dq_{\text{irrev.}}$$

$$\therefore \left( \Delta S = \frac{dq_{\text{rev.}}}{T} \right)$$

$$0 > dq_{\text{irrev.}} - Tds \quad \text{---(1)}$$

$$(dq_{\text{irrev.}})_P = dH \quad \text{---(2)}$$

Put the value of (2) in (1)

$$0 > dH - Tds$$

$$0 > (dq)_{T,P}$$

Gibbs-Helmholtz Equation

we know that

$$G = H - TS$$

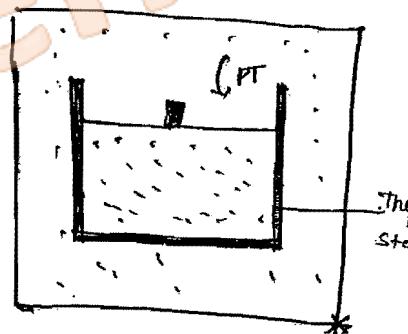
For initial  $\rightarrow$

$$G_1 = H_1 - TS_1 \quad \text{---(1)}$$

$$\text{for final, } G_2 = H_2 - TS_2 \quad \text{---(2)}$$

at constant temp. &

$$\Delta G = \Delta H - T \Delta S \quad \text{---(3)}$$



$$dG = Vdp - SdT$$

$$\left(\frac{dq}{dT}\right)_P = -S$$

for initial

$$\left(\frac{dq_1}{dT}\right)_P = -S_1 \quad \textcircled{4}$$

for final

$$\left(\frac{dq_2}{dT}\right)_P = -S_2 \quad \textcircled{5}$$

Subtract  $\textcircled{5} - \textcircled{4}$

$$\left(\frac{d(\Delta G)}{dT}\right)_P = -\Delta S \quad \textcircled{6}$$

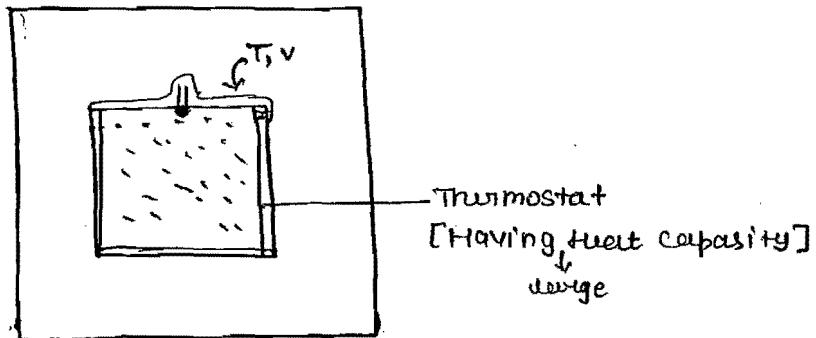
Put the value of  $\textcircled{3}$  in  $\textcircled{6}$

$$\left(\frac{d(\Delta G)}{dT}\right)_P = \frac{\Delta G - \Delta H}{T}$$

$$T \cdot \left(\frac{d(\Delta G)}{dT}\right)_P + \Delta H = \Delta G$$

$\Leftarrow$  Gibbs-Helmholtz Equation  $\Rightarrow$

## Helmholtz function



for  $- (T, V)$

work - function

or  
Helmholtz function or 'A'

$$A = E - TS$$

↓ disorder

Energy

- ⇒ It is a Energy function
- ⇒ It is also Extensive property
- ⇒ It Unit Expresses in Joule
- ⇒ It is also called work function and represented by  $A'$
- ⇒ When a system undergoing change at a constt volume then their Energy expression term in internal Energy & when you subtract disorder from total Energy, we get Helmholtz free Energy or work function.
- ⇒ for spontaneous  $(dA)_{T,V} < 0$

→ Comparison b/w Helmholtz free Energy and Gibbs free Energy

\* For an Isothermal Process, for an ideal Gas ( $\Delta G = \Delta A$ )

$$G = H - TS$$

$$G = E + PV - TS$$

$$dG = dE + PdV + VdP - TdS - SdT \quad [ \because dT = 0 ]$$

$$dG = dA + TdS + SdT + PdV - VdT - TdS - SdT \quad [ \because A = E - TS ]$$

$$dG = dA + \delta(P, V)$$

$$\therefore dA = dE - TdS - SdT$$

$$\delta G = dA + \delta(C, T) \quad [ \because PV = RT ]$$

$$dG = dA + RdT \quad [ \because \delta T = 0 ]$$

$$dG = dA$$

To prove  $\Rightarrow$

$$\Delta A = \Delta E + T \left( \frac{\partial (\Delta A)}{\partial T} \right)_V$$

## Partial Molar Property $\Rightarrow$

Suppose  $Z$  is a function of  $\rightarrow$

$$Z = f(T, P, n_1, n_2, n_3, \dots, n_i)$$

= Where System having different mole of gases  
 $(n_1, n_2, n_3, \dots, n_i)$

$\Rightarrow$  The Total diff. of  $Z \rightarrow$

$$dZ = \left( \frac{\partial Z}{\partial T} \right)_{P, n_1, n_2, n_3, \dots, n_i} dT + \left( \frac{\partial Z}{\partial P} \right)_{T, n_1, n_2, n_3, \dots, n_i} dP$$

$$+ \left( \frac{\partial Z}{\partial n_1} \right)_{P, T, n_2, \dots, n_i} dn_1 + \left( \frac{\partial Z}{\partial n_2} \right)_{T, P, n_1, n_3, \dots, n_i} dn_2$$

at const.  $T, + P$

$$dZ = \left( \frac{\partial Z}{\partial n_1} \right)_{T, P, n_2, n_3, \dots, n_i} dn_1 + \left( \frac{\partial Z}{\partial n_2} \right)_{T, P, n_1, n_3, \dots, n_i} dn_2 + \left( \frac{\partial Z}{\partial n_3} \right)_{T, P, n_1, n_2, n_4, \dots, n_i} dn_3$$

$$dZ = \boxed{\left( \frac{\partial Z}{\partial n_i} \right)_{T, P, n_1, n_2, \dots, (n_i-1)}}$$

$\Downarrow$  Partial molar property

this is called P.m.P. bcoz  $\Delta Z [G_i, E, A] \uparrow$  (with change in  $i^{th}$ ) component of the system where all other component are constant.

Note:  $\Rightarrow$  (i) The properties which occurs in the pure state of the system is different for the impure system

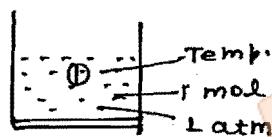
(Pure state)

e.g. When we adding one mole of water  $100\text{cm}^3$  of pure water when we get  $\Delta V = 18\text{cm}^3$ . bcoz (one mole of water =  $18\text{cm}^3$ )

... in the gaseous state when we adding a 1 mole of  $H_2O$  the

2(i) the change in property in gmpure state is arises due to bcoz of different interaction take place.

## CHEMICAL POTENTIAL



$$\mu_i^\circ = \frac{g}{n}$$

$\mu_i \Rightarrow$  (temp. dependent)



$$\mu_i = \left( \frac{\partial g}{\partial n_i} \right)_{T, P, n_1, n_2, \dots, (n_{i-1})}$$

$$\mu_i = \left( \frac{\partial g}{\partial n_i} \right)_{T, P, n_2, \dots, n_i}$$

$$\mu_2 = \left( \frac{\partial g}{\partial n_2} \right)_{T, P, n_1, n_3, \dots, n_i}$$

$$\mu_3 = \left( \frac{\partial g}{\partial n_3} \right)_{T, P, n_1, n_2, \dots, n_i}$$

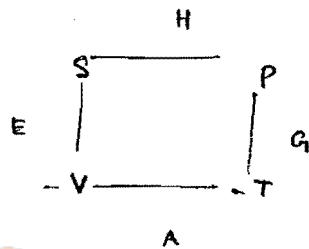
⋮

- Change in free energy with change in particular component in a system which containing diff. no. of moles where all other moles are constant
- Gibb's free energy changes with the change in particular component at constant T & P where all other component are constant that is ~~is~~ ~~suppose~~ chemical potential.

- for a pure state free energy per mole is called chemical potential. Standard chemical potential can be defined for a pure state of a compound, amount 1 mole, 1 atmosphere at any temp. then it is called standard chemical potential.  
 $[\mu^\circ] = G/n$
- Standard chemical potential only depends upon temp. while chemical potential of a particular component in a gmpure state depends upon T & P both.

$\mu = \mu^\circ + RT \ln P_i$	→ in term of partial pressure
$\mu = \mu^\circ + RT \ln X_i$	→ in terms of mole fraction

Chemical potential can also be represented in diff. thermodynamically.



$$\left(\frac{\partial A}{\partial N_i}\right)_{V,T} = \mu_i$$

$$\left(\frac{\partial H}{\partial N_i}\right)_{S,P} = \mu_i$$

$$\left(\frac{\partial G}{\partial N_i}\right)_{P,T} = \mu_i$$

$$\left(\frac{\partial E}{\partial N_i}\right)_{S,V} = \mu_i$$

#  $\Rightarrow$  Variation of chemical potential with temperature #

{  $\therefore G$  decreases with temp,  $\therefore \frac{dG}{dT} < 0$  }

$\therefore \mu$  also be  $\downarrow$  with temp

$\Rightarrow$  [लेट्रफॉन त्रांसफर के  $\mu_i$  समीक्षा]

we know that  $\Rightarrow$

$$\left(\frac{\partial G}{\partial N_i}\right)_{T,P} = \mu_i$$

$$\frac{d}{dT} \left( \frac{\partial G}{\partial N_i} \right) = \frac{\partial \mu_i}{\partial T}$$

$$\frac{\partial^2 G}{\partial T \partial N_i} = \frac{\partial \mu_i}{\partial T} \quad \text{---(1)}$$

$$\therefore dG = vdp - SdT$$

$$\left(\frac{\partial f}{\partial T}\right)_P = -S$$

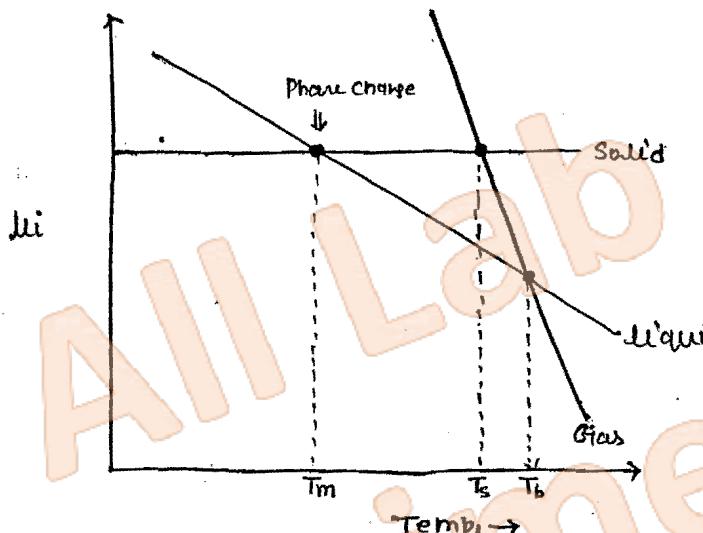
by ① and ⑪

$$\frac{\partial^2 G}{\partial n_i \partial T} = - \left(\frac{\partial S}{\partial n_i}\right)$$

$$\frac{\partial^2 G}{\partial n_i \partial T} = - \bar{S}_i \quad \text{--- ⑫}$$

$$\boxed{\left(\frac{\partial \mu_i}{\partial T}\right)_P = -\bar{S}_i}$$

Gate-2010



$T_s$  = Sublimation temp.

$T_b$  = Boiling temp.

$T_m$  = Melting temp.

Graph:  $\Rightarrow$  Variation of chemical potential with change in temp.

$\Rightarrow$  during phase transition chemical potential remain  $\downarrow$  same for both the phases.  
[where  $T, V, \epsilon$  all other component are constant],

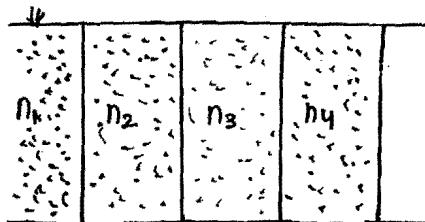
$\Rightarrow$  since we know that  $G$  is state function so it must follow

Euler's theorem.

$$\boxed{\left(\frac{\partial (\mu_i)}{\partial T}\right)_P = -\bar{S}_i}$$

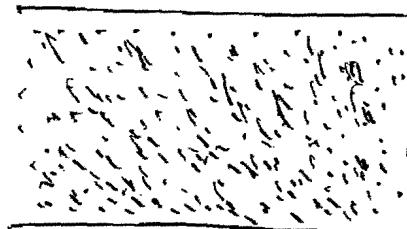
# # Calculation of thermodynamic parameter [ $\Delta H^{\text{mixing}}$ , $\Delta V^{\text{mix}}$ , $\Delta S^{\text{mix}}$ , $\Delta A^{\text{mix}}$ ] In the case of ideal gases

2) 4 compartment system



(Before mixing)

(After removing compartment)  
[सारे compartment को open कर दिया जाएगा]



(After mixing)

$n_1$  [Pure state] \*

$$\mu_1^\circ = \frac{G_1}{n_1}$$

$$n_2, \mu_2^\circ = \frac{G_2}{n_2}$$

$$n_3, \mu_3^\circ = \frac{G_3}{n_3}$$

$$n_4, \mu_4^\circ = \frac{G_4}{n_4}$$

$$\mu_1 = \mu_1^\circ + RT \ln x_1$$

$$\mu_2 = \mu_2^\circ + RT \ln x_2$$

$$\mu_3 = \mu_3^\circ + RT \ln x_3$$

$$\mu_4 = \mu_4^\circ + RT \ln x_4$$

$$G_{\text{Total}} = n_1 \mu_1 + n_2 \mu_2 + n_3 \mu_3 + n_4 \mu_4$$

[After mixing]

$$G_{\text{Total}} = n_1 \mu_1^\circ + n_2 \mu_2^\circ + n_3 \mu_3^\circ + n_4 \mu_4^\circ$$

[Before mixing]

$$\Delta G^{\text{mixing}} = \frac{G_{\text{Total}} \text{ (After mixing)}}{G_{\text{Total}} \text{ (Before mixing)}}$$

$$\begin{aligned}
 &= (n_1 \mu_1 + n_2 \mu_2 + n_3 \mu_3 + \dots) - (n_1 \mu_1^\circ + n_2 \mu_2^\circ + n_3 \mu_3^\circ + \dots) \\
 &= n_1 (\mu_1^\circ + RT \ln x_1) + n_2 (\mu_2^\circ + RT \ln x_2) + n_3 (\mu_3^\circ + RT \ln x_3) \\
 &\quad + \dots - (n_1 \mu_1^\circ + n_2 \mu_2^\circ + \dots) \\
 &= n_1 RT \ln x_1 + n_2 RT \ln x_2 + \dots
 \end{aligned}$$

2

$$\Delta G_{\text{mix}} = RT \sum n_i \ln x_i$$

$$\frac{\Delta G_{\text{mix}}}{T} = R \sum n_i \ln x_i$$

$$\frac{\partial}{\partial T} \left[ \frac{\Delta G_{\text{mix}}}{T} \right]_P = \frac{\partial}{\partial T} \left( \sum n_i \ln x_i \right)_P$$

$$-\frac{\Delta G_{\text{mix}}}{T^2} + \frac{1}{T} \left( \frac{\partial (\Delta G_{\text{mix}})}{\partial T} \right)_P = 0 \quad \text{--- (1)}$$

$$\therefore \Delta G_{\text{mix}} = \Delta H_{\text{mix}} + T \left( \frac{\partial (\Delta G_{\text{mix}})}{\partial T} \right)_P$$

Divide both side by  $T^2$  then,

$$\frac{\Delta G_{\text{mix}}}{T^2} = \frac{\Delta H_{\text{mix}}}{T^2} + \frac{1}{T} \left( \frac{\partial (\Delta G_{\text{mix}})}{\partial T} \right)_P$$

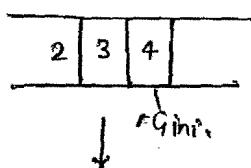
$$-\frac{\Delta H_{\text{mix}}}{T^2} = -\frac{\Delta G_{\text{mix}}}{T^2} + \frac{1}{T} \left( \frac{\partial (\Delta G_{\text{mix}})}{\partial T} \right)_P \quad \text{--- (2)}$$

By Eq.n - (1) + (2)

$$-\frac{\Delta H_{\text{mix}}}{T^2} = 0$$

$\Delta H_{\text{mix}} = 0$

e.g. 2 mol O<sub>2</sub>, 3 mol N<sub>2</sub>, 4 mol H<sub>2</sub>



$$n_{\text{Total}} = 9$$

$$\Delta f.$$

$$\Delta G = Q_f - Q_i$$

$$\Delta G_{\text{mix.}} = RT \left( 2 \ln \frac{2}{9} + 3 \ln \frac{3}{9} + 4 \ln \frac{4}{9} \right)$$

(Per mole)

$$= RT \left[ \left( \frac{2}{9} \right) \ln \left( \frac{2}{9} \right) + \frac{3}{9} \ln \left( \frac{3}{9} \right) + \frac{4}{9} \ln \left( \frac{4}{9} \right) \right]$$

Rxn & kinetic energy ( $\Delta E_f$ )  $\rightarrow \uparrow \text{temp.} \rightarrow K, E, P, E, \Rightarrow$

$$\Delta G_{\text{mix.}} = \frac{RT \sum n_i \ln x_i}{n_{\text{Total}}}$$

$$\Delta G_{\text{mix.}} = RT \sum x_i \ln x_i$$

(Per mole)

Q4.8

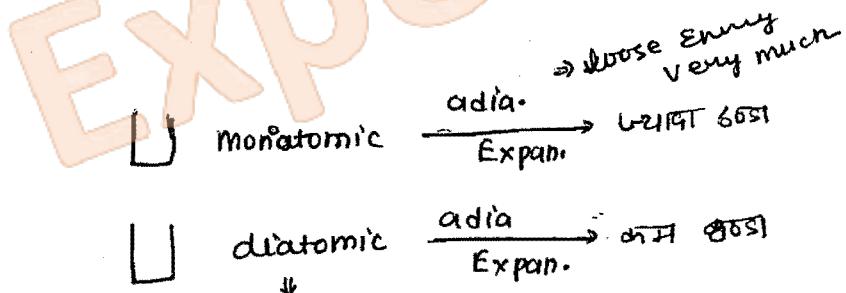
2 mole of N<sub>2</sub>

3 mole of H<sub>2</sub>

2 mole of NH<sub>3</sub>

$$\begin{aligned}
 \Delta S_{\text{mixing}} &= 8.314 \times \left[ \frac{2}{7} \ln\left(\frac{2}{7}\right) + \left(\frac{3}{7}\right) \ln\left(\frac{3}{7}\right) + \left(\frac{2}{7}\right) \ln\left(\frac{2}{7}\right) \right] \\
 &= 8.314 \times 2.303 \times \left[ 2 \log \frac{2}{7} + 3 \log \frac{3}{7} + 2 \log \left(\frac{2}{7}\right) \right] \\
 &= 8.314 \times 2.303 \times \left[ 4 \log \frac{2}{7} + 3 \log \frac{3}{7} \right] \\
 &= -8.314 \times 2.303 \times \left[ -0.9462 + (-0.36 \times 3) \right] \\
 &= -8.314 \times 2.303 \times [-2.9462 - 1.089] \\
 &= -8.314 \times 2.303 \times (-3.830) \\
 &= 62.80 \text{ J K}^{-1}
 \end{aligned}$$

Q4.9



No. of atom  $\propto$  Rotation, vibration

No. of atom  $\propto$  Heat capacity \*

$$\therefore T_m < T_p < T_i$$

monatomic  $\Rightarrow$  Temp. independent.

(3)

$$\Delta G_{\text{mixing}} = \Delta H_{\text{mixing}}^{\circ} - T \cdot \Delta S_{\text{mixing}}$$

$$\Delta G_{\text{mixing}} = -T \cdot \Delta S_{\text{mixing}}$$

$$\Delta S_{\text{mixing}} = -\frac{\Delta G_{\text{mixing}}}{T}$$

$$\Delta S_{\text{mixing}} = -R \sum n_i \ln x_i$$

$$\Delta S_{\text{mixing, per mole}} = -R \sum x_i \ln x_i$$

$$\Delta G_{\text{mixing}} = \Delta A_{\text{mixing}}$$

[bcz isothermal]  $\Rightarrow$  Ideal working substance

→ When ideal Gases mixing with each other since there is no interaction b/w the molecule so there is no absorption or rejection of heat take place so that  $\Delta H = 0$

$$\boxed{\Delta H_{\text{mixing}} = 0}$$

(if there is no interaction  
No interaction  
No work Energy)

Q4: One mole of  $\text{CO}_2$ , one mole of  $\text{NO}_2$  & two mole of  $\text{O}_2$  were mixed at 300K calculate the Entropy of mix.,  $\Delta H_{\text{mixing}}$   $\Delta V_{\text{mixing}}$ ,  $\Delta A_{\text{mixing}}$

1 mole of  $\text{CO}_2$

1 mole of  $\text{NO}_2$

2 mole of  $\text{O}_2$

$$\Delta G = -RT \left[ 1 \ln \frac{1}{4} + 1 \ln \frac{1}{4} + 2 \ln \frac{2}{\#_2} \right]$$

$$\Delta G = RT \left[ 2 \ln \frac{1}{4} + 2 \ln \frac{1}{2} \right]$$

$$\Delta G = RT \times 2.303 \left[ 2 \ln \frac{1}{4} + 2 \ln \frac{1}{2} \right]$$

$$\Delta G = 8.314 \times 300 \times 2.303 \times [-2 \times (0.60) - 2 \times (0.30)]$$

$$= 8.314 \times 300 \times 2.303 \times [-1.2 - 0.6]$$

$$= 8.314 \times 300 \times 2.303 \times [-1.8]$$

$$= -10,374$$

$$\boxed{\Delta H_{\text{mix.}} = 0}$$

$$\Delta G = \Delta A = -10,374$$

$$= -10,374 \text{ KJ}$$

$$\Delta G = -\frac{\Delta G}{T} = +34.58 \text{ J}$$

$$\boxed{\Delta V_{\text{mixing}} = 0}$$

09L

$$\Delta S = 6R \ln 2$$

$$\ln \frac{k_2}{k_1} = \frac{E_g}{R} \left[ \frac{T_2 - T_1}{T_1 \cdot T_2} \right] \quad \text{Arrhenius Eqn}$$

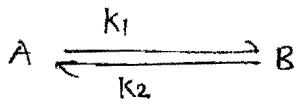
[in term of rate constant]

$$\ln \frac{k_{P_1}}{k_{P_2}} = \frac{\Delta H^\circ}{R} \left[ \frac{T_2 - T_1}{T_1 \cdot T_2} \right] \quad \text{in term of } k_p \text{ [Equi. constt]}$$

Vant-Hoff Relation

$$\ln \frac{k_{C_1}}{k_{C_2}} = \frac{\Delta E^\circ}{R} \left[ \frac{T_2 - T_1}{T_1 \cdot T_2} \right] \quad \text{[in term of } k_c \text{]}$$

⇒ For Chemical Equilibrium first condition → system must be closed. [It is Dynamic in Nature]



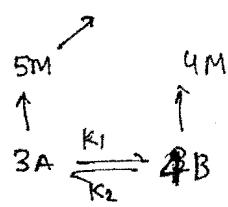
$K \Rightarrow$

$K_x \Rightarrow$

$K_p \Rightarrow$

$K_c \Rightarrow$

$(K_p \neq K_c)$  may or may not depend upon stoichiometry  
mean depends upon stoichiometry



$$\alpha = \frac{S_m}{1M} = S$$

unitless (mole fraction)  
(always)

$$K_x = \frac{(X_B)^4}{(X_A)^3}$$

$$\frac{k_1}{k_2} = K_c = \frac{[c_B]^4}{[c_A]^3}$$

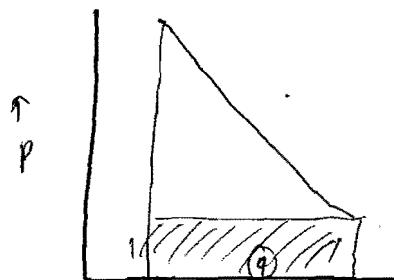
$$K_p = \frac{[P_B]^4}{[P_A]^3} \quad \text{(in A mixture)}$$

$K$  = thermodynamic equi. (unitless)  
= always

always

Ignore

Q4.21



Rev:

$$\text{Rev} = \frac{1}{2} \times 4 \times 4 + 4 \times 1 \\ 8 + 4 = 12 \quad [x]$$

$$\text{Touch} = 1 \times 4 = 4 \text{ L.atm}$$

$$\frac{\partial}{\partial T} (\ln k_p) = \frac{\Delta H^\circ}{RT^2}$$

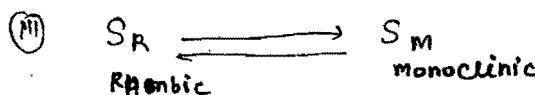
$$\frac{\partial}{\partial T} (\ln k_e) = \frac{\Delta E^\circ}{RT^2}$$

### -: CLAUSIUS - CLAYPERON RELATION

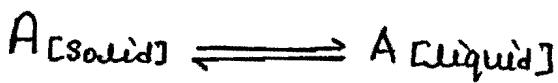
[Phase-transformation]  $\therefore \Delta q = 0$  [at Equilibrium]  
 chemical potential  $= 0$  ]- (bcz at Equi.)  
 $\therefore \Delta G = 0$

Clausius Clayperon Equation is applying for any phase transformation a phase transformation which is a immediate process, during this the temp., pressure, equilibrium conc., free Energy of two different phases etc. are equal.

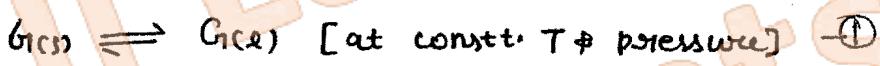
For e.g.  $\Rightarrow$  There is a lot of phase transfer



for Solid-Liquid Equi.



Note: Solid changes into liquid at their melting point during this they absorb heat at a constt. pressure from the surrounding. During this phase transformation the sign of heat absorbed is +ve.  
[अगर लिक्विड से solid बाता हो -ive]



At a slight increase of temp. ( $T + dT$ ,  $P + dP$ ).



from (I) & (II)

$$dG(s) \rightleftharpoons dH(l)$$

applying Maxwell Equation  $\rightarrow$

~~dH(l)~~

$$V(g)dP - S_{(s)}dT = V(l)dP - S_{(l)}dT$$

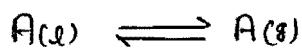
$$\frac{dP}{dT} = \frac{\Delta S}{V_{(l)} - V_{(s)}} \quad \text{---(III)}$$

Here integrated form  
not possible bcz we  
neglect (s) &

$$\therefore \Delta S = \frac{\Delta H}{T} \quad \text{---(IV)}$$

$$\left[ \frac{dP}{dT} = \frac{\Delta H}{T} \right]$$

Differential form of



$$\therefore G(l) \rightleftharpoons G(g) \quad [\text{at const. } T, P] \quad \text{---(i)}$$

when you slightly increases the  $(T + \delta T, P + \delta P)$  then,

$$G(l) + \delta G(l) \rightleftharpoons G(g) + \delta G(g) \quad \text{---(ii)}$$

from I & II Ind -

$$\delta G(l) \rightleftharpoons \delta G(g)$$

$$\therefore \delta G = Vdp - SdT \quad [\text{Maxwell equation}]$$

$$V(l)dp - S(l)dT = V(g)dp - S(g)dT$$

$$\frac{dp}{dT} = \frac{\Delta S}{V(g) - V(l)}$$

$$\Delta S = \frac{\Delta H}{T}$$

$$\boxed{\frac{dp}{dT} = \frac{\Delta H}{T} (V(g) - V(l))}$$

$\downarrow$   
Diff. form of Clapeyron Eqn

$\because V_g \ggggg \gg V(l)$

$$\frac{dp}{dT} = \frac{\Delta H}{T \times V(g)}$$

$$\frac{\partial P}{\partial T} = \frac{\Delta H \times P}{T \times RT} \quad [\because PV = RT], \quad V = \frac{RT}{P}$$

$$\frac{\partial P}{\partial T} = \frac{\Delta H \cdot P}{RT^2}$$

Integrated on both side

$$\int_{P_1}^{P_2} \frac{dp}{p} = \frac{\Delta H}{R} \int_{T_1}^{T_2} \frac{dT}{T^2}$$

$$\ln \frac{P_2}{P_1} = \frac{\Delta H^\circ}{R} \left[ \frac{T_2 - T_1}{T_1 \cdot T_2} \right]$$